

# Application Shale Rating System to Hambalang Hill Clayshale Performance

*by Putera Agung M.a*

---

**Submission date:** 27-Apr-2022 09:27AM (UTC+0700)

**Submission ID:** 1821458809

**File name:** Proceeding\_TEC\_ASAIS\_2017\_2\_Putera\_Agung.pdf (2.58M)

**Word count:** 3099

**Character count:** 17910

## Application Shale Rating System to Hambalang Hill Clayshale Performance

**16** Putera Agung M Agung, Suripto S

Civil Engineering, Politeknik Negeri Jakarta

Jl Prof.Dr.GA Siwabessy, Kampus Baru UI Depok 16425

email : putera\_agung2002@yahoo.com

### Abstract

A "shale rating system" based on durability, strength; and plasticity proposed by Franklin et al (1971) is applied for clayshale of Hambalang Hill. Several result for durability; strenght; and plasticity were collected and analyzed to investigate the clayshale from study area in Hambalang based on the shale rating system. From study, Hambalang shale has the shale rating starts from 0 (zero) to 7 (seven); they have a cohesion ( $c'$ ) value between 10 to 50 kPa; an angle internal friction ( $\phi'$ ) between 2.5 to 24.0°; and a critical slope angle between 10 to 35°. Durability ( $I_d$ ) is lower than 55%; they have an undrained shear strength ( $S_u$ ) between 20 – 30 kg/cm<sup>2</sup> and clayshale modulus between 10 to 20 MPa; and also an allowable bearing capacity between 2.0 to 4.0 MPa. The clayshale can be classified into stiff clay to very low rock class.

**Keywords:**clayshale, shale rating system,durability, strength; plasticity.

### 1. INTRODUCTION

Shales constitute about one-third of the rocks in the land surface of the earth and about one-half by volume of all sedimentary rocks. Not surprisingly, they are common in engineering projects either in their excavated form as construction materials in their natural and undisturbed state. In spite of its abundance, this important rock type has until recently received little attention. In some ways, it is an unattractive and difficult material to study because it is easily disturbed during drilling, sampling, and specimen preparation. The strength, deformability and other characteristics of a laboratory test specimen can change by orders of magnitude if the rock is allowed to dry out, shrink, or swell.

A further experimental problem is that, whereas the minerals and microtexture of most rocks can be studied easily by using standard optical methods, extremely

fine-grained clay minerals require techniques such as scanning electron microscopy or X-ray diffraction (Putera et al, 2017). Shales also vary greatly in their properties and behavior. At some locations shale slopes stand for many years at near-vertical angles, whereas at others even 10-20° slopes suffer from continual erosion and creep. This has led to a distinction between clayshales, the softer and more soil-like types, and indurated-shales, which, because of their greater cementation and compaction, behave more like harder rocks. The practice of treating shales as either a soil-like or rock-like material has been carried into construction specifications, where payment has often been based on a distinction between soil and rock. Problems have occurred with shales of intermediate quality that behave neither as soil nor as hard rock and require special treatment. There is a clear need for a shale classification system that is capable of distinguishing all grades and qualities of shale and allows a

correlation between the type of shale and its performance on engineering projects. A rating number R is assigned to a shale according to measurements of the three properties considered fundamental to distinguish one shale from another: durability, strength, and plasticity. Tentative correlations have been developed between the rating number and aspects of engineering performances such as excavating methods; foundation properties; and slope stability, especially relations between slope height and angle and mechanisms of failure in different types of shale). The suggested correlations are based on limited data, and their value and accuracy will improve with use and experience. Nevertheless, it is believed that in their present form they serve to illustrate trends of behavior and will stimulate further research into the performance of this important group of materials.

## 2. THEORY

Size-strength classification before considering the subject of shale characterization, it may be helpful to discuss briefly the classification of rocks in general. Of the many characteristics of a rock mass, two in particular appear to be important in determining rock – mass behavior in engineering works: (a) the size of blocks into which the rock mass is divided by intersecting sets of joints and other discontinuities and (b) the intrinsic strength of these blocks. Some classifications, such as that published by Bieniawski (1974) and Barton (1974), include a greater number of classification parameters and as a result are somewhat more difficult to apply. The two-parameter approach has been found to be a useful starting point and one that is readily

comprehended and used. The size-strength classification is insufficient, however, when applied to shales or other rocks of limited durability. A sample of shale excavated from the rock mass initially plots at a single location on the diagram; this location depends on the size and strength of rock fragments. When the shale is exposed to weathering, however, it becomes weaker or breaks down to smaller-sized fragments. The effects of short-term weathering processes can be recorded on the diagram in the form of vectors that represent weakening, disintegration or a combination of the two processes. Different shales vary in their susceptibility to short-term weathering agencies, and a measure of this susceptibility is essential in characterizing shale materials for engineering projects.

Hambalang hill is an intrusion area of igneous rock (Fig. 1). Geologically, intrusion will emerge when tectonic force works, (fault). Infrastructure built on fault area have susceptibility to landslides and ground movements. A number of landslides are always occurred in Hambalang hill area. Geomorphology of the Hambalang area consists of fluvial plain; steep volcanic; steep cliff; steep karst; ramps; and sedimentary hills rather steep to steep. Based on lithography aspect, Hambalang hill area is divided into five units of rock from the oldest to the youngest at early Miocene claystone, early Miocene limestone, andesite middle Miocene and Holocene alluvium. The tectonic activity of the Miocene-Pliocene period causes folding, fault, and breakthrough (Martodjojo, 1984). The direction of the main compression firm in Hambalang hill relatively northwest-northwest, southwest-north-northeast and north-south

direction. Endogenous process causing Hambalang area to become mainland, while exogenous activity at causing the rocks to erode.

Shale sample was collect from Hambalang hillarea, West Java at coordinates 6°33'16" south latitude and 106°53'22" east longitude. Sample core was carried out at 9,0 to 21.0 m depth using the diamond head boring machine. Standard of tube sampler was used for all undisturbed samples and some core boxes were used to monitor undisturbed samples. For At the shale layers was also from 2.5 to 21.0 m performed standard penetration of field test (SPT) to evaluate the number of blow (N-SPT). Shale layer has number of blow more than 50, so these layers were very stiff and coloured from light to dark grey (Putera Agung et al, 2013).

From soil mechanics laboratory by using the macro testing, analytical results of core samples show that soil properties of Hambalang shales have specific gravity ( $G_s$ ) in the range between 2.62 to 2.65. By using the Atterberg limits test was found that liquid limit (LL) equals 31.75%, plastic limit (PL) equals 21.87%, and plasticity index (PI) = 9.88%. Grain size analysis shows that the material composition consists of silt (86.2%); clay (10%); and sand (3.8%). Thus, it indicates that silt soil type dominates of Hambalang shales. Clay mineral content of Hambalang shales are chiefly illite, with minor kaolinite. Illite content ranges from 7.8% to 90.8%; those of kaolinite, 18.7 % to 95.6%. This reflects the Hambalang shales were formed in the middle period of diagenesis and clay mineral of illite fraction is generally the highest. Hambalang shales is mainly controlled by sedimentation and consolidation process, residual soil

type of weather rocks at the origin, weathering and erosion in the source area, transport processes and to the depositional environment. Each shale has a different depositional history and clay diagenesis is influenced by many different. Hambalang shales indicates similar characteristics has low porosity and permeability (Putera et al, 2016).

### 3. METHODOLOGY

The proposed shale rating system is shown in Fig. 2, the shale rating chart. A sample of shale is given a rating number on the basis of (a) its slake durability and strength if the shale is rocklike and has a slake-durability index greater than 80 percent or (b) its slake durability and plasticity if the shale is 'soil-like' and has a slake-durability index less than 80 percent.

Samples are initially subjected to the slake-durability test to assess their second - cycle slake durability index ( $I_{d2}$ ) in percent, in accordance with ISRM recommended procedures. If this index is found to exceed 80 percent, the sample is further tested to measure the point-load-strength index. If the index is less than 80 percent, the fraction passing the slake-durability test drum (Fig. 3) is subjected to conventional Atterberg-limits determinations to evaluate plasticity index.

18

The point-load-strength test has been found to be convenient for strength classification of rocks in general and of shales in particular. It requires no specimen preparation or machining and can be conducted in the field before the rock has had a chance to dry or break up. The index used for rating purposes is the strength obtained when the load is applied perpendicular to the bedding planes

(for the strongest direction). Supplementary measurements can be made with the load applied parallel to the bedding planes to measure strength anisotropy and fissility. Samples are tested at their natural, moisture content. Point-load-strength values have been found to correlate closely with those obtained in the uniaxial compressive strength test. For classification purposes uniaxial strengths can be obtained by applying a factor of 24 to the point load strength values (Broch and Franklin, 1972).

### 3. ANALYSIS AND DISCUSSION

Figure 4 shows the test results obtained for samples of shales collected in Hambalang hill as part of the current research program. The results have been subdivided according to the geologic age of the formation tested. It can be seen that older formations, as expected, are generally stronger and more durable and have higher rating values. Perhaps the most characteristic feature of this diagram, however, is the considerable scatter in durability, strength, and rating values for the majority of formations. The scatter reflects real differences in shale properties as a result of differing degrees of lithification and of in-situ weathering. Evidently the character of these materials differs significantly from place to place throughout the province and even from bed to bed within a single formation. The index test results therefore give important additional information and the characteristics of these shales cannot be inferred from rock or formation names alone.

It may be noted that Hambalang shales are generally less durable and weak. Hambalang shales are dominated by detrital minerals

(quartz), clay minerals (mainly illite and kaolinite). From evidence of XRD test (Putera, et al, 2015) shales at shallow depths and low temperatures, hydrous minerals such as illite and kaolinite form as a result of weathering or early diagenetic processes during meteoric water flow. Such early diagenetic processes may be considered a continuation of the weathering process even if the porewater is reducing.

The main primary minerals such as quartz are unstable when exposed to meteoric water of low ionic strength near the surface (weathering), but comprise a stable mineral assemblage during burial diagenesis at higher temperatures and lower flow rates. It is well known that arkoses have their quartz well preserved after exposure to greenschist facies or higher grades of metamorphism. Only if kaolinite potentially unstable clay minerals form at shallow depth will clay mineral reactions such as precipitation of illite take place at greater burial due to higher temperatures. In such well-sorted reservoir sandstones, nearly all the clay minerals are authigenic and the distribution of clay minerals then depends on the diagenetic processes.

Several observations were carried out in the laboratory of soil mechanics to find a relationship between XRD in the micro and strength properties in the macro analysis. Based on slope stability analysis, slope safety factor (SF) indicated that the value exists in the range of 1.04 to 1.12. Critical heights from safety factor equals 1.0 is 4.30 m. The existing slope condition is susceptible to collapse or landslide when the high rainfall intensity occurred or the natural water content exceeds over 35% since the clay mineral (especially illite) absorbs

the excessive water. Excessive pore water pressure causes the clay shale loss of cohesion. Then, illite will reduce the permeability easily and leads to the high pore water pressure exceeding total stress, and effective stress can be decreased. Furthermore, unstable kaolinite potential to separate clay mineral entirely and damage to soil bonding structure due to lower temperature and water existing around the quartz fractions. Climatic conditions in Hambalang hill area also has the highest intensity for rainfall in rainy season, especially in the southern of Jakarta, so that the area can allow the landslide. Thus far, there are several mechanisms which cause or affect shale/fluid interaction. There is an intense effort under way in the construction project to get a better understanding of each of these mechanisms. The stakes are high in that understanding and quantification of each of these phenomena is critical for foundation design which would stabilize shales. Rapid progress is being made and more results will become available in the near future. The current understanding of various mechanisms responsible for shale and water interaction indicate certain basic principles for improving foundation system to improve shale stability and bearing capacity at studi area (Fig. 5).

The long-term stable angle of a slope in shale can vary from about 80 to almost vertical depending on the durability of the shale material. Different slope failure mechanisms occur in shales that have different rating values. In shales of low durability mechanisms of slaking, erosion, and surface creep predominate. Unprotected steep slopes exposed to continual erosion by surface runoff rainwater develop a pattern of erosion gulleys. The surface

layer slakes, and the debris is removed by erosion as fast as it is produced. Although there is usually no safety hazard associated with this mechanism, periodic cleaning of ditches is required, and the appearance of the exposed eroded rock can be unattractive. Slopes that are protected from continuous erosion develop a weathering profile.

Instability of the surface layer is encouraged if undercutting occurs at the toe of the slope. It is also accentuated by water percolation along the contact between weathered and unweathered materials. The surface layer is usually more clayey and less permeable than the underlying rocks and thus traps water. Eventually, a clay slope will reach a stable angle equal to approximately half the residual angle of shearing resistance of the material (Bjerrum, 1976).

Allowable bearing pressure is generally controlled by, and can be estimated from, the intact rock strength and the intensity of jointing or bedding (the size strength parameters). In view of difficulties in making field measurements of joint defines three values for the empirical coefficient that depend only on major variations in the spacing of discontinuities: very wide, wide, and moderately close (Canadian Foundation Manual, 1978).

#### 4. CONCLUSION

Illite and kaolinite play an important role to decrease cohesion, and quartz acts as a medium water flow. Thus, shales in Hambalang hill more stable against sliding than after exposed to water. The correlation between illite and or kaolinite and porosity of the shale is not good. The quantification of the impact of water

invasion on effective stresses and shale strength is critical for shale stability analysis models. Both minerals of shale are very hard to release the water between and intra particle and contribute to produce the high excess pore water pressure exceeding the total stress, and induces the micro fissure.

Hambalang hill slope failures are generally more common in shales that have lower ratings. In these shales, the sliding surface may pass through intact shale material and there may be only limited influence from preexisting bedding and jointing. In the harder more durable shales, slope failures are invariably controlled by the orientations of preexisting discontinuity sets. Wedge or planar slides are bounded by slicking surfaces coincident with preexisting joints and bedding planes.

Foundation modulus is generally very low and not relevant to the design of heavily loaded structures. The foundation modulus of argillaceous rocks generally increases from clay shale modulus between 10 to 20 MPa; and also an allowable bearing capacity between 2.0 to 4.0 MPa. The clay shale can be classified into stiff clay to very low rock class.

## 5. CONCLUSION

- [1] Bieniawski, Z.I. (1974). Geomechanics Classification of Rock Masses and Its Application in Tunneling. Proceeding of the 3rd International Congress on Rock Mechanics, Denver, Vol. 2a, 1974, pp. 27-32.
- [2] Barton, N, Lien, R., and Lunde, J. (1974). Engineering Classification of Rock Masses for the Design of Tunnel Support. Rock Mechanics, Vol. 5, No. 4, pp. 189-236.
- [3] Bjerrum, L. (1976). Progressive Failure in Slopes of Overconsolidated Plastic Clay and Clay Shales. Proceeding of Journal of Soil Mechanics and Foundations Division, American Society of Civil Engineers, New York, Vol. 93, No. SM5, pp. 1-49.
- [4] Broch, E and Franklin, J.A. (1972). The Point-Load Strength Test. International Journal of Rock Mechanics and Mining Sciences, Vol. 9, 1972, pp. 669-697.
- [5] Canadian Geotechnical Society. (1978). Canadian Foundation Manual.
- [6] Franklin, A, Broch, E and Walton, G. (1971). Logging the Mechanical Character of Rock. Trans. Institute of Mining and Metallurgy (Great Britain), Vol. 80, 1-971, pp. A1-49.
- [7] Gamble, J.C. (1975). Durability-Plasticity Classification of Shales and Other Argillaceous Rocks. Univ. of Illinois, Urbana-Champaign, Ph.D. thesis.
- [8] Martodjojo, S. (1984). Evolusi Cekungan Bogor Jawa Barat. Disertasi Doktor Geologi, Fakultas Pasca Sarjana, Institut Teknologi Bandung.
- [9] Putera Agung, M.A, Suropto, and Dandung, N. Mineral Characteristics and their Geological Significance of Shales in Southern Jakarta by X-ray Diffraction Analysis. Prosiding Seminar Nasional Teknik Infrastruktur dan Lingkungan, Mitigasi dan Pemulihan Kondisi Pasca Bencana Alam, Politeknik Negeri Manado, pp. 22-29.
- [10] Putera Agung, MA; Damianto, B; Yuwono; Istiatun (2013). A Critical State Approach to Stability of Clayshale for Design Structures of the Sentul Hill, West Java, Indonesia. Proceeding of the 4th International Conference of the Euro-Asia Civil Engineering Forum, National University of Singapore (NS), pp. G – 7.
- [11] Putera Agung, MA, Yuwono, Mursid, Sutikno (2017). Micro Testing (XRD; SEM; Petrography)

for Clayshale Layer, Indonesia.  
 Lambert Publishing Academic.  
 [12] Van Bemmelen, R.W. (1949). The  
 Geology of Indonesia, Volume I A.  
 The Hague: MartinusNijhoff,  
 Netherland. Adams B, Alden J, and

Harris N (2006) Regional  
 development and spatial planning in  
 an enlarged European Union.  
 Aldershot: Ashgate.

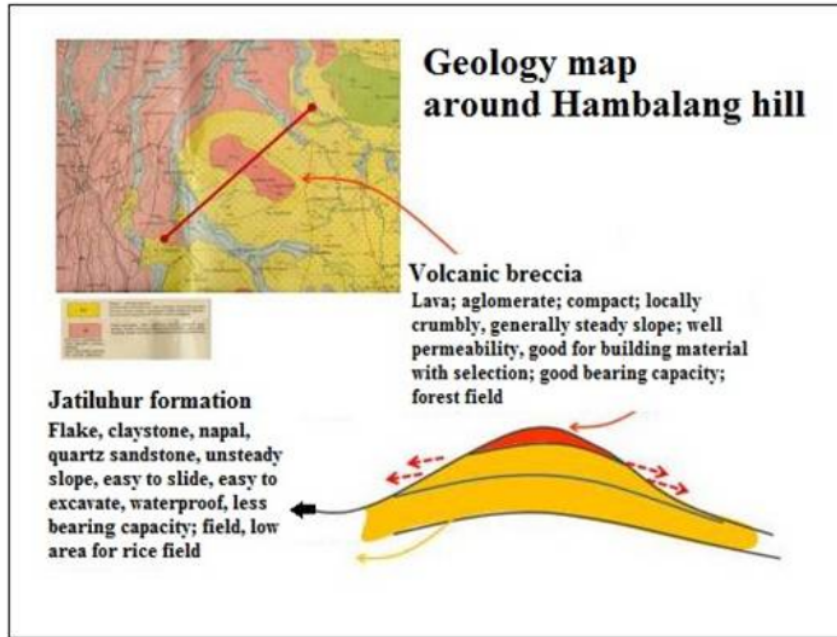


Fig. 1 Geology map (Bemmelen, 1949)

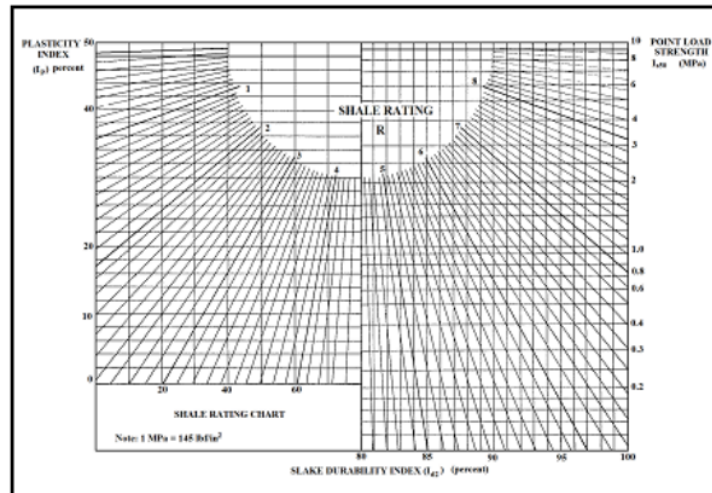


Fig. 1 Shale rating chart (Gamble, 1975)



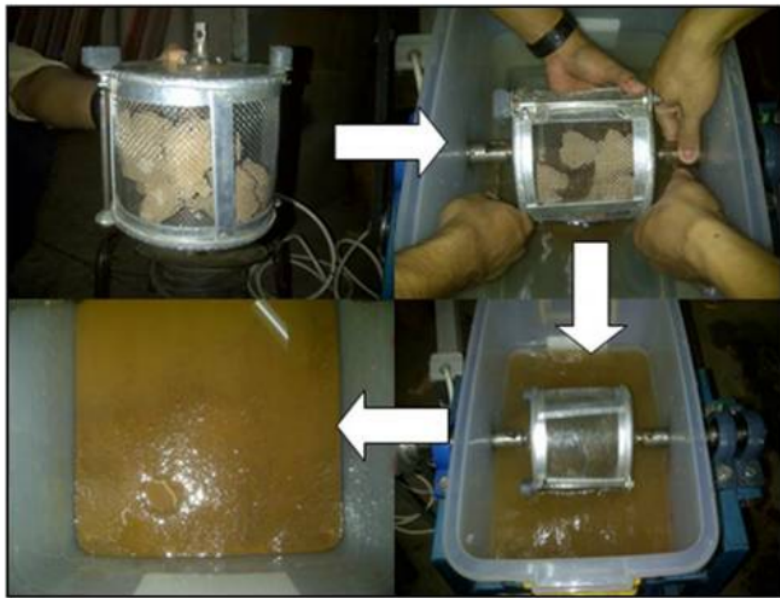


Fig. 2 Slake – durability test

PROBABILITY GEOLOGICAL AGE	SLAKE DURABILITY INDEX PERCENT $I_{42}$	POINT LOAD STRENGTH INDEX (MPa) $I_{ps0}$	SHALE RATING R
	0 20 40 60 80 100	.2 .4 .6 .8 1 2 4 6 8 10	1 3 5 7 9
EARLY MIOCENE (youngest claystone)			
EARLY MIOCENE (oldest claystone)			
EARLY MIOCENE (limestone)			
MIDDLE MIOCENE (andesite)			
MIDDLE HOLOCENE (alluvium)			

Fig. 4 Relation between age and index properties

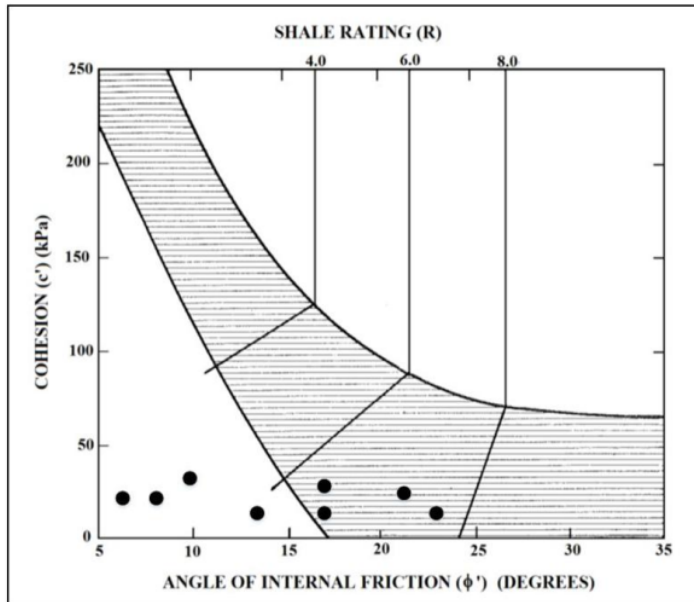


Figure 7. Trends in shear-strength parameters of nature of Hambalang clayshale

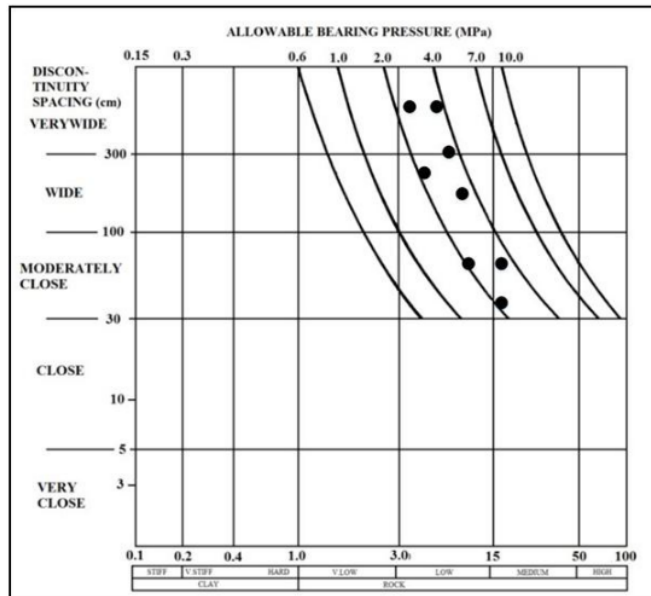


Fig. 10 Allowable bearing pressure for Hambalang clayshale

ISSN 2302-786X

# Application Shale Rating System to Hambalang Hill Clayshale Performance

---

## ORIGINALITY REPORT

---

14%

SIMILARITY INDEX

10%

INTERNET SOURCES

11%

PUBLICATIONS

8%

STUDENT PAPERS

---

## PRIMARY SOURCES

---

1

[www.unud.ac.id](http://www.unud.ac.id)

Internet Source

1%

---

2

Osama M. Elnaggar, Mostafa G. Temraz. "Lower Paleozoic reservoir zonation into different flow units using turbulence factor and their relations to diagenesis", Journal of Petroleum Exploration and Production Technology, 2017

Publication

1%

---

3

R Azsarinka, D Saleh, E Djonaedi. "Synthesis of biodegradable plastic from corn starch and corn husk filler with addition of glycerol as plasticizer and variation of chitosan composition", IOP Conference Series: Materials Science and Engineering, 2020

Publication

1%

---

4

[pustaka.unpad.ac.id](http://pustaka.unpad.ac.id)

Internet Source

1%

---

5

[slidelegend.com](http://slidelegend.com)

Internet Source

1%

---

6	Submitted to University of Witwatersrand Student Paper	1 %
7	Submitted to University of Brighton Student Paper	1 %
8	T. Y. Irfan, G. E. Powell. "Études géologiques pour fondations par pieux dans un granite profondément altéré à Hong Kong", Bulletin of the International Association of Engineering Geology, 1985 Publication	1 %
9	W Diana, E Hartono, A S Muntohar. "The Permeability of Portland Cement-Stabilized Clay Shale", IOP Conference Series: Materials Science and Engineering, 2019 Publication	1 %
10	Submitted to Curtin University of Technology Student Paper	1 %
11	Gercek, H.. "Poisson's ratio values for rocks", International Journal of Rock Mechanics and Mining Sciences, 200701 Publication	1 %
12	<a href="http://eprints.unsri.ac.id">eprints.unsri.ac.id</a> Internet Source	1 %
13	<a href="http://www.scielo.org.za">www.scielo.org.za</a> Internet Source	1 %

14 Fuqiang Gao, Doug Stead, Hongpu Kang. "Numerical investigation of the scale effect and anisotropy in the strength and deformability of coal", International Journal of Coal Geology, 2014  
Publication 1 %

---

15 eprints.utm.my  
Internet Source 1 %

---

16 ojs.pnb.ac.id  
Internet Source <1 %

---

17 www.ijrte.org  
Internet Source <1 %

---

18 Peter George Fookes, William Robert Dearman, John Allan Franklin. "Some engineering aspects of rock weathering with field examples from Dartmoor and elsewhere", Quarterly Journal of Engineering Geology and Hydrogeology, 1971  
Publication <1 %

---

19 Broch, E.. "The point-load strength test", International Journal of Rock Mechanics and Mining Sciences and Geomechanics Abstracts, 197211  
Publication <1 %

---

20 geoinfo.nmt.edu  
Internet Source <1 %

---

---

Exclude quotes Off

Exclude matches Off

Exclude bibliography Off